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CATADIOPTRIC IMAGING SYSTEM EMPLOYING IMMERSION LIQUID
FOR USE IN BROAD BAND MICROSCOPY

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CATADIOPTRIC IMAGING SYSTEM EMPLOYING IMMERSION LIQUID
FOR USE IN BROAD BAND MICROSCOPY

This application is a continuation-in-part of U.S. Patent Application Serial No. 10/646,073, 5 entitled "Catadioptric Imaging System for Broad Band Microscopy," inventors David G. Shafer, et al., filed August 22, 2003, which is a continuation-in-part of U.S. Patent Application Serial No. 10/434,374, entitled "High Performance Catadioptric Imaging 10 System," inventors David G. Shafer, et al., filed May 7, 2003, which claims the benefit of U.S. Provisional Patent Application Serial No. 60/449,326, entitled "High Performance, Low Cost Catadioptric Imaging System," filed February 21, 2003.

15 BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates generally to the field of optical imaging and more particularly to catadioptric optical systems used for microscopic 20 imaging, inspection, and lithography applications.

Description of the Related Art

Many optical systems have the ability to inspect or image features on the surface of a specimen, such as inspecting defects on a semiconductor wafer or 25 photomask, or alternately examining a biological specimen on a slide. Microscopes have been used in various imaging situations, including biology, metrology, semiconductor inspection, and other complex

inspection applications where high resolution images of small areas and/or features are desired.

Typically available imaging systems include microscopes, which use offer inspection using dry imaging, or imaging in a gaseous medium such as air. Many newer applications either require or may benefit from immersion imaging. Unlike dry imaging, immersion imaging immerses the sample in water or other liquid and images or inspects the image within the liquid.

Immersion imaging can, in certain circumstances, provide increased optical properties, including but not limited to enhanced resolution, over dry imaging. Furthermore, due to the nature and fragile properties associated with certain biological specimens, biological imaging systems frequently cannot use dry imaging whatsoever. In this situation, a biological imaging system can only image a sample while the sample is immersed in liquid, necessitating the use of a system able to perform immersion imaging.

Problems with immersion imaging and objectives employed within immersion imaging systems include the ability to resolve the image using immersion imaging operation in the presence of either low wavelength or broad wavelength range light energy, successfully employing different types of illumination and imaging modes, and effective objective usage in widely available standard equipment, such as microscopes.

Microscopes designed to support immersion imaging can be difficult to design for high resolution

specimen imaging. To improve the quality of the image received, such a system may use various imaging modes to enhance the appearance of desired features on the specimen. Imaging modes used in an immersion imaging system may include bright field, dark field, differential interference contrast, confocal, and other imaging modes offering different benefits depending on the type of specimen, the features on the specimen being observed, the imaging environment, and other related considerations.

Certain imaging modes may employ light energy of varying wavelengths, and thus the ability to effectively resolve images and operate in the presence of a wide variety of wavelengths and over various wavelength ranges may be particularly beneficial. For immersion imaging, the system objective is one of the most critical components of the design and may use light having a broad range of wavelengths, including wavelengths below 400 nm. Some available UV objectives can transmit light at wavelengths down to a wavelength of 340 nm, but these objectives do not provide accurate imaging performance for light wavelengths below the range of approximately 400 nm. These types of objectives are mainly used for fluorescence, where wavelengths from 340 nm through the visible light spectrum excite fluorescence components in marker dyes. The fluorescent emission for these objectives is typically in the visible light spectrum, so imaging performance in the visible light spectrum is the specific type of performance required.

Such fluorescence excitation does not perform an inspection of the specimen and thus such an objective provides limited, if any, inspection functionality.

The ability for an objective to operate within a standard microscope is both desirable and difficult to achieve for the detailed inspection performance required for semiconductor and biological inspections discussed above. No immersion objectives are currently known that can support broad band inspection performance at light wavelengths below 400 nm. Some dry objective designs may be highly corrected for broad band imaging at wavelengths below 400 nm, but none of these dry objective designs can be used in a standard microscope system. The dry objective designs are typically too large, have insufficient numerical aperture (NA), or have an insufficient field size.

It would therefore be beneficial to provide a system and objective for use in conjunction with standard microscopes and microscopy applications that overcome the foregoing drawbacks present in previously known dry imaging/immersion imaging systems. Further, it would be beneficial to provide an optical inspection system design having improved functionality over devices exhibiting the negative aspects described herein.

SUMMARY OF THE INVENTION

According to a first aspect of the present invention, there is provided an objective employed for use in inspecting a specimen. The objective is
5 employed with light energy having a wavelength in a range of approximately 266 to 1000 nanometers. The objective comprises a focusing lens group comprising at least one focusing lens configured to receive the light energy and form focused light energy, a field
10 lens oriented to receive focused light energy from the focusing lens group and provide intermediate light energy, a Mangin mirror arrangement positioned to receive the intermediate light energy from the field lens and form controlled light energy, and an
15 immersion liquid between the Mangin mirror arrangement and the specimen.

According to a second aspect of the present invention, there is provided an objective employed for use in inspecting a specimen. The objective comprises
20 a focusing lens group configured to receive light energy and comprising at least one focusing lens, and at least one field lens oriented to receive focused light energy from the focusing lens group and provide intermediate light energy, a Mangin mirror arrangement positioned to receive the intermediate light energy from the field lens and form controlled light energy,
25 and an immersion substance located between the Mangin mirror arrangement and the specimen. The Mangin mirror arrangement imparts the controlled light energy
30 to the specimen with a numerical aperture in excess of

0.9 and a field size of greater than or equal to approximately 0.15 mm.

According to a third aspect of the present invention, there is provided a method for inspecting a specimen. The method comprises providing light energy having a wavelength in the range of approximately 157 nanometers through the infrared light range, focusing the light energy using at least one lens into focused light energy, where each lens used in the focusing has a diameter less than approximately 100 millimeters, receiving the focused light energy and converting the focused light energy into intermediate light energy, and receiving the intermediate light energy and providing controlled light energy through an immersion substance to a specimen.

According to a fourth aspect of the present invention, there is provided a variable focal length optical system for use in the presence of an objective having an objective exit pupil. The variable focal length optical system is employed in inspecting a specimen. The variable focal length optical system comprises a relatively fixed focusing lens group configured to receive the light energy from the exit pupil of the objective and comprising at least one focusing lens, and at least one movable imaging lens group oriented to receive focused light energy from the focusing lens group and provide an image. Each movable imaging lens group is capable of being repositioned relative to the relatively fixed focusing lens group, and separation between the relatively

fixed focusing lens group and the exit pupil of the objective enables insertion of additional optical elements.

These and other objects and advantages of the
5 present invention will become apparent to those skilled in the art from the following detailed description of the invention and the accompanying drawings.

DESCRIPTION OF THE DRAWINGS

The present invention is illustrated by way of example, and not by way of limitation, in the figures of the accompanying drawings in which:

5 FIG. 1 illustrates an aspect of the catadioptric objective design similar to that presented in FIG. 1 of U.S. Patent 5,717,518;

FIG. 2 is an aspect of the catadioptric objective design similar to that presented in FIG. 4 of U.S.

10 Patent 6,483,638;

FIG. 3 presents a nine element reduced size catadioptric immersion objective with a 0.95 NA in accordance with the present design, corrected over a bandwidth from 266 to 436 nm and having a field size
15 of approximately 0.150 mm;

FIG. 4 is a broad band reduced size catadioptric immersion objective with a 1.0 NA in accordance with the present immersion imaging design, corrected over a bandwidth from 266 to 436 nm and having a field size
20 of approximately 0.150 mm;

FIG. 5 illustrates a nine element reduced size catadioptric immersion objective with a 1.0 NA in accordance with the present design, corrected over a bandwidth from 190 to 196 nm and having a field size
25 of approximately 0.150 mm;

FIG. 6 presents a ten element reduced size catadioptric immersion objective with a 1.2 NA in

accordance with the present design, corrected over a bandwidth from 190 to 196nm and a substantially flat immersion surface;

FIG. 7 illustrates an eleven element reduced size
5 catadioptric immersion objective with a 1.1 NA in accordance with the present design, corrected over a bandwidth from 266 to 436 nm and having a field size of approximately 0.150 mm;

FIG. 8 is a eight element reduced size
10 catadioptric immersion objective with a 1.2 NA in accordance with the present design, corrected over a bandwidth from 190 to 198 nm and having a field size of approximately 0.050 mm;

FIG. 9 shows a catadioptric objective design
15 corrected for a 0.17 mm thick cover glass and can be adjusted correct for variations in the thickness of the cover glass;

FIG. 10 is a self corrected varifocal imaging system with a 50 to 300x magnification range;

20 FIG. 11 is a "figure 4" mirror arrangement for use with the varifocal imaging system.

FIG. 12 is a "trombone" type mirror arrangement for use with the varifocal imaging system.

DETAILED DESCRIPTION OF THE INVENTIONAvailable Dry Imaging Designs

Two patents that disclose dry objective, broad band, highly UV corrected, high numerical aperture 5 (NA) catadioptric systems are U.S. Patent 5,717,518 to Shafer et al. and U.S. Patent 6,483,638 to Shafer et al. Both represent dry imaging designs having certain advantageous inspection and imaging characteristics. A representative illustration of a catadioptric design 10 100 in accordance with the teachings of the '518 patent is presented in FIG. 1, which is similar to FIG. 1 of the '518 patent. A representative illustration of a catadioptric design 200 in accordance with the teachings of the '638 patent is 15 presented in FIG. 2, which has similarities to FIG. 4 of the '638 patent.

U.S. Patent 5,717,518 to Shafer et al. discloses a dry objective design capable of high NA, ultra broadband UV imaging. The high NA (up to 20 approximately 0.9) system can be used for broadband bright field and multiple wavelength dark-field imaging. Certain issues exist with designs similar to that presented in FIG. 1. First, the field lens group may need to be physically located within a central 25 hole in the large curved catadioptric element, which can make manufacturing difficult and expensive. Second, the field lens elements in such a design may require at least one glued interface. In the presence of wavelengths less than 365nm, reliable glues that

can withstand light intensity levels at an internal focus are generally unavailable. Third, the lens elements in such a design may be located very close to a field plane, thereby requiring a high degree of, or
5 nearly perfect, surface quality and bulk material quality to prevent image degradation. Fourth, element diameters are typically larger than a standard microscope objective, especially for the catadioptric group. Large diameter elements prevent integration
10 into a standard microscope system.

The dry objective design of FIG. 2 is generally capable of high NA, ultra broadband UV imaging. The design is a high NA (up to approximately 0.9) imaging system that can be used for broadband bright field and
15 multiple wavelength dark-field imaging and can use a varifocal tube lens to provide a large range of magnifications. The FIG. 2 design introduces very tight tolerances in the field lens group, due in part to increased on-axis spherical aberration produced by
20 the catadioptric group. This on-axis spherical aberration must be corrected by the following refractive lens elements. The design of FIG. 2 is relatively large, thereby generally requiring complicated optomechanical mounting of elements,
25 especially in the catadioptric group.

With respect to NA, the NA of an objective represents the objective's ability to collect light and resolve fine specimen detail at a fixed object distance. Numerical aperture is measured as the sine
30 of the vertex angle of the largest cone of meridional

rays that can enter or leave the optical system or element, multiplied by the refractive index of the medium in which the vertex of the cone is located. A large numerical aperture provides distinct advantages
5 during inspection, not the least of which is an ability to resolve smaller features of the specimen. Also, high NAs collect a larger scattering angle, thereby improving performance in darkfield environments. For this reason, immersion objectives
10 with high NAs are very desirable, and it is typically beneficial to specify the immersion substance refractive index when determining the operating NA of the objective. Changing the immersion substance to one having a higher refractive index will
15 proportionally increase the NA.

An objective that can cover as large a range of wavelengths as possible is also desirable in certain scenarios, particularly when using an arc lamp as an illumination source. Currently available immersion
20 designs are all refractive, and refractive designs tend to limit wavelength range because few glass materials having high transmission below 400nm are effective for chromatic correction.

Small objectives are also desirable, as small
25 objectives can be used in combination with standard microscope objectives and physically fit within standard microscope turrets. The standard objective flange-to-object distance is in the range of 45mm. The available catadioptric objectives frequently
30 cannot satisfy this requirement, so special microscope

systems can be employed having an objective flange-to-object distance in excess of 60 mm and having lens diameters greater than 60 mm.

An objective having low intrinsic aberrations is
5 also desirable, as is an objective that is largely self-corrected for both monochromatic and chromatic aberrations. A self corrected objective will have looser alignment tolerances with other self corrected imaging optics. An objective with loose manufacturing
10 tolerances, such as lens centering tolerances, may be particularly beneficial. Further, reducing incidence angles on lens surfaces can have a large effect on optical coating performance and manufacturing. In general, lower angles of incidence on lens surfaces
15 also produce looser manufacturing tolerances.

Immersion Imaging Designs

The present design presents a catadioptric immersion objective corrected over a wide wavelength range using a single glass material, or in certain
20 circumstances, more than one glass material to improve performance. The objective employed herein may provide particular benefits in the microscopy field. One aspect of the objective design is shown in FIG. 3. The catadioptric objective as shown in FIG. 3 is
25 optimized for broad-band imaging in the UV and visible spectral region, namely approximately 0.266 to 0.436 micron wavelengths. The objective provides high numerical apertures of 0.95 assuming pure water is used as an immersion substance. Other immersion

substances could be used with higher indices to further increase the NA. The inventive design presented uses the Schupmann principle in combination with an Offner field lens to correct for axial color
5 and first order lateral color. As shown in the aspect presented in FIG. 3, the field lens group 302 is slightly displaced from the intermediate image 315 to obtain enhanced performance, and the design employs liquid as shown by immersion liquid layer 313.

10 As used herein, the terms "immersion liquid," "immersion substance," or "immersion liquid layer" refer to any non-solid non-gaseous substance, including but not limited to liquid or other viscous material, as particularly differentiated from gasses
15 or gaseous materials. Immersion liquids that may be employed in the current design include, but are not limited to, water, oil, silicone gel, or other liquid, semi-liquid, viscous, or partially viscous substances. While solid, gaseous, or other materials may be
20 included within the "immersion liquid" or "immersion substance," as used herein, these materials comprise primarily liquid, semi-liquid, viscous, or partially viscous substances. These terms will be used throughout this discussion primarily using the term
25 "immersion liquid," but use of the other terms such as immersion substance or immersion liquid layer indicates materials conforming to the definition presented herein.

From FIG. 3, the catadioptric group 303 or Mangin
30 mirror arrangement includes a Mangin mirror element

312. Mangin mirror element 312 is a reflectively coated lens element. The catadioptric group 303 also includes concave spherical reflector 311, also a reflectively coated lens element. Both elements in
 5 the catadioptric group 303 have central optical apertures where reflective material is absent. The absence of reflective material allows light to pass from the object or specimen 314 through the immersion liquid 313 to Mangin mirror element 312, reflect from
 10 the second or outer surface of concave spherical reflector 311, onto the reflective surface of Mangin mirror element 312, and through concave spherical reflector 311 to form an intermediate image 315 after concave spherical reflector 311. The field lens group
 15 302 may comprise one or more lenses, and in the aspect shown in FIG. 3, one field lens 310 is employed.

The focusing lens group 301 uses multiple lens elements, in the aspect shown six lens elements 304, 305, 306, 307, 308, and 309. All lenses in the
 20 focusing lens group 301 may be formed from a single type of material to collect the light from the field lens group 302 and the intermediate image 315.

The lens prescription for the aspect of the invention illustrated in FIG. 3 is presented in Table
 25 1.

Table 1. Prescription for lenses for the design of FIG. 3

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.00
1	Infinity	18.0000		9.10

STO	Infinity	-18.0000		8.50
3	17.6779	2.0000	Fused Silica	9.08
4	-44.7675	0.5000		8.85
5	13.6362	1.2500	Fused Silica	8.33
6	5.9607	5.6987		7.45
7	-6.5395	2.3911	Fused Silica	7.54
8	-12.2563	0.5000		8.78
9	29.8365	2.0000	Fused Silica	9.28
10	-21.5455	0.5000		9.40
	-			
11	101.8361	2.0000	Fused Silica	9.34
12	-24.8901	0.5000		9.32
13	6.7391	2.2500	Fused Silica	8.81
14	22.9759	7.8495		8.19
15	1.9529	1.2495	Fused Silica	2.50
16	6.1579	0.7828		1.66
17	Infinity	0.9995		0.00
18	18.1935	4.1697	Fused Silica	26.20
19	12.8633	5.7334		21.20
20	183.2127	4.4199	Fused Silica	21.20
21	-91.4932	-4.4199	MIRROR	21.20
22	183.2127	-5.7334		21.20
23	12.8633	-4.1697	Fused Silica	21.20
24	18.1935	4.1697	MIRROR	26.20
25	12.8633	5.7334		21.20
26	183.2127	4.4199	Fused Silica	0.00
27	-91.4932	0.4862	Fused Silica	0.00
IMA	Infinity		Fused Silica	40.00

As may be appreciated by one skilled in the art, the numbers in the leftmost column of Table 1 represent the surface number counting surfaces from the left of FIG. 3. For example, the left surface of lens 304 in the orientation presented in FIG. 3 (surface 3 in Table 1) has a radius of curvature of 17.6779 mm, a thickness of 2.0 mm, and the rightmost surface (surface 4) has a radius of curvature of -44.7675mm, and is 0.5mm from the next surface. The material used is fused silica, and surface 3 has a diameter of 9.08 mm while surface 4 has a diameter of 8.85 mm.

In the design presented in FIG. 3, the numerical aperture may approach or even exceed approximately 0.95 in water. From FIG. 3, the focusing lens group 301 has the ability to receive light energy and 5 transmit focused light energy. The field lens group 302 has the ability to receive the focused light energy and provide intermediate light energy, and form intermediate image 315. The catadioptric group or Mangin mirror arrangement 303 receives the 10 intermediate energy and provides controlled light energy to the specimen. Alternately, the reflected path originates at the specimen, and light reflected from the specimen is received by the catadioptric group or Mangin mirror arrangement 303 and forms and 15 transmits reflected light energy. The field lens group 302 receives the reflected light energy and transmitting resultant light energy, and the focusing lens group receives resultant light energy and transmits focused resultant light energy. An aperture 20 or mask can be placed at the aperture stop (not shown) to limit or modify the NA of the objective.

The design presented in FIG. 3 and Table 1 thus uses a single glass material, fused silica. Other materials may be employed, but it is noted that fused 25 silica or any material used within the design may require low absorption over the range of wavelengths supported by the objective design. Fused silica offers relatively high transmission properties for light energy from 190 nm through the infrared 30 wavelengths. Because of the single material design of

the immersion objective, fused silica can enable the design to be re-optimized for any center wavelength in this wavelength range. For example, the design can be optimized for use with lasers at 193, 198.5, 213, 244,
5 248, 257, 266, 308, 325, 351, 355, or 364nm. The design can also be optimally employed to cover lamp spectral bands from 190-202, 210-220, 230-254, 285-
320, and 365-546nm. In addition, if calcium fluoride is employed as a glass or lens material, the design
10 can be employed with an excimer laser at 157 nm or excimer lamps at 157 or 177nm. Re-optimization requires slight tuning or altering of components, and may generally be within the abilities of those skilled in the art. Calcium fluoride lenses may also be
15 employed in the field lens group to increase the bandwidth of the objective.

The maximum diameter of a lens element is 26 millimeters, which is significantly smaller than many objective designs previously employed in this
20 wavelength range. The small size of this objective is particularly beneficial in view of the performance characteristics of the objective. As a result, the objective can be mounted in a standard microscope turret with an approximate 45mm flange-to-object separation.
25 This immersion objective supports a numerical aperture of approximately 0.95, a field size of approximately 0.15 mm, has a corrected bandwidth from approximately 266-436 nm, and a polychromatic wavefront error of less than approximately 0.05 waves,
30 levels which had been previously unachievable in

combination in a single design. Field size in this arrangement represents the size of the area on the specimen that can be imaged the system with minimum degradation in optical performance.

5 As is true with any optical design, certain tradeoffs may be made to improve performance characteristics depending on the desired application of the objective or optical design. It is possible, for example, to sacrifice bandwidth, field size,
10 numerical aperture, and/or objective size to enhance one of the aforementioned performance characteristics, depending on the application. For example, optimizing for lower or higher NAs is possible. Reducing the NA can reduce the manufacturing tolerance and the outer
15 diameter of the objective. Lower NA designs can provide larger field sizes and larger bandwidths. Lower NA designs with the same performance and less optical elements are also possible. Optimizing for higher NAs is also possible. Optimizing the design
20 for higher NAs would generally limit the field size or bandwidth and may require slightly increased diameter objective elements.

The design of FIG. 3 provides a relatively low intrinsic polychromatic wavefront aberration over the
25 design bandwidth from approximately 266-436nm. The low wavefront aberration provides increased manufacturing headroom, or ease of manufacture, while enabling relatively high performance of the manufactured objective. The design is also self
30 corrected, where self corrected in this context means

that the objective does not require any additional optical components to correct aberrations in order to achieve inspection design specifications. In other words, no additional components are needed to provide

- 5 a generally aberration free image, or the objective provides substantially complete images without need for additional compensation. The ability to self correct can provide for simpler optical testing metrology and optical alignment to other self
10 corrected imaging optics. Further correction of residual aberrations using additional imaging optics is also possible, where further correction can increase the optical specifications, including but not limited to bandwidth or field size.

15 The design of FIG. 3 has relatively loose tolerances on the refractive index of the glass material, largely due to use of a single material that does not rely on the refractive index difference of two different glass materials to compensate for
20 chromatic aberrations. Use of a single material also makes the design very insensitive to temperature changes. Previous designs have used multiple glass materials with different refractive index profiles for color correction. The result is the refractive index
25 profile for each material changing differently with temperature, thereby changing the chromatic correction for temperatures other than the design temperature and reduced overall performance.

30 The immersion objective design presented herein can support various modes of illumination and imaging.

Modes supported can include bright field and a variety of dark field illumination and imaging modes. Other modes such as confocal, differential interference contrast, polarization contrast may also be supported
5 using the present design.

Bright field mode is commonly used in microscope systems. The advantage of bright field illumination is the clarity of the image produced. Using bright field illumination with an objective such as that presented
10 herein provides a relatively accurate representation of object feature size multiplied by the magnification of the optical system. The objective and optical components presented herein can be readily used with image comparison and processing algorithms for
15 computerized object detection and classification.

Bright field mode typically uses a broad band incoherent light source, but it may be possible to use laser illumination sources with slightly modified illumination system components and employing the objective design
20 presented herein.

The confocal mode has been used for optical sectioning to resolve height differences of object features. Most imaging modes have difficulty detecting changes in the height of features. The confocal mode
25 forms separate images of object features at each height of interest. Comparison of the images then shows the relative heights of different features. Confocal mode may be employed using the design presented herein.

Dark field mode has been used to detect features on objects. The advantage of the dark field mode is that flat specular areas scatter very little light toward the detector, resulting in a dark image. Surface features 5 or objects protruding above the object tend to scatter light toward the detector. Thus, in inspecting objects like semiconductor wafers, dark field imaging produces an image of features, particles, or other irregularities on a dark background. The present design may be 10 employed with dark field mode illumination. Dark field mode provides a large resultant signal upon striking small features that scatter light. This large resultant signal allows larger pixels to be employed for a given feature size, permitting faster object inspections. 15 Fourier filtering can also be used to minimize the repeating pattern signal and enhance the defect signal to noise ratio during dark field inspection.

Many different dark field modes exist, each including a specific illumination and collection scheme. 20 Illumination and collection schemes can be chosen such that the scattered and diffracted light collected from the object provides an acceptable signal-to-noise ratio. Certain optical systems use different dark field imaging modes including ring dark field, laser directional dark 25 field, double dark field, and central dark ground. Each of these dark field imaging modes may be employed in the present design.

Any of the above mentioned imaging modes may be efficiently employed with the immersion imaging design 30 of FIG. 3, albeit where slight modifications to certain

components may offer improvements to certain performance parameters. In any configuration, the immersion imaging objective design presented enables inspection in any of the named imaging modes with the result of a relatively

- 5 high numerical aperture, operation over a broad wavelength spectrum, with relatively high field size. The design can operate within a standard microscope turret and offers imaging performance better than that previously known.

10 An alternate aspect of the present design presents an immersion objective with nine separate elements. This aspect of the design is presented in FIG. 4. The differences between the design of FIG. 4 and that of FIG. 3 are the reoptimization to correct
15 for the refractive index and dispersion of water used as the immersion fluid. The design of FIG. 4 also increases the NA of the objective to approximately 1.0 assuming pure water is used as an immersion substance. Other immersion substances could be used with higher
20 refractive indices to further increase the NA. The objective of the design of FIG. 4 is corrected over a bandwidth from approximately 266 to 436 nm has a field size of approximately 0.150 mm. The worst case polychromatic wavefront error for the FIG. 4 design is
25 approximately 0.05 waves.

From FIG. 4, the catadioptric group 403 includes a Mangin mirror element 412, which is a reflectively coated lens element, and a concave spherical reflector 411, which is also a reflectively coated lens element.
30 Both Mangin mirror element 412 and concave spherical

reflector 411 have central optical apertures where reflective material is absent. The absence of reflective material, in the center of the components shown, allows light to pass from the object or

5 specimen 414, through the immersion liquid 413, and Mangin mirror element 412, reflect from the second surface of concave spherical reflector 411 onto the Mangin mirror element 412, and transmit through concave spherical reflector 411 to form an

10 intermediate image 415 after concave spherical reflector 411. Field lens group 402 comprises a single field lens 410 in this aspect of the design.

The focusing lens group 401 employs multiple lens elements, in this aspect the six lens elements 404, 405, 406, 407, 408, and 409, which may all be formed from a single type of material. The focusing lens group 401 collects light from the field lens group 402, including the intermediate image 415. An aperture or mask can be placed at the aperture stop 20 (not shown) to limit or modify the NA of the objective. The design presented in FIG. 4 has virtually all of the advantages and flexibility described with respect to the design of FIG. 3. The lens prescription for this embodiment is shown in

25 Table 2.

Table 2. Prescription for lenses for the design of
FIG. 4

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.00
1	Infinity	19.0000		9.13
STO	Infinity	-19.0000		8.50
3	28.5196	2.0000	Fused silica	9.12
4	-33.6705	0.5000		8.95
5	12.9081	1.2500	Fused silica	8.48
6	6.5008	6.6131		7.70
7	-6.9274	2.1444	Fused silica	7.76
8	-14.7698	0.5000		8.88
9	35.7354	2.0000	Fused silica	9.37
10	-22.7923	0.5000		9.53
11	88.0026	2.0000	Fused silica	9.52
12	-32.4362	0.5000		9.47
13	7.2825	2.2500	Fused silica	9.01
14	28.2840	8.3107		8.41
15	2.0231	1.2495	Fused silica	2.60
16	7.4344	0.8873		1.80
17	Infinity	0.9995		0.63
18	17.7330	4.1250	Fused silica	26.00
19	12.4735	5.6276		21.00
20	127.4223	4.1943	Fused silica	20.00
21	-105.0674	-4.1943	MIRROR	20.00
22	127.4223	-5.6276		20.00
23	12.4735	-4.1250	Fused silica	21.00
24	17.7330	4.1250	MIRROR	26.00
25	12.4735	5.6276		21.00
26	127.4223	4.1943	Fused silica	20.00
27	-105.0674	0.6026	WATER	20.00
IMA	Infinity		WATER	20.00

An alternate aspect of the present design
5 presents an immersion objective again having nine
elements. This aspect of the design is presented in
FIG. 5. The main difference between the design of
FIG. 5 and that of FIG. 3 is the redesign for a
shorter wavelength while maintaining a relatively high
10 1.0 numerical aperture assuming pure water is used as

an immersion substance. Other immersion substances could be used with higher refractive indices to further increase the NA. The objective of the design of FIG. 5 is corrected over a bandwidth from 5 approximately 190 to 196 nm and has a field size of approximately 0.150 mm. The worst case polychromatic wavefront error for the FIG. 5 design is approximately 0.04 waves.

From FIG. 5, the catadioptric group 503 includes 10 a Mangin mirror element 512, again a reflectively coated lens element, and a concave spherical reflector 511, which is also a reflectively coated lens element. Both Mangin mirror element 512 and concave spherical reflector 511 have central optical apertures where 15 reflective material is absent. The absence of reflective material, in the center of the components shown, allows light to pass from the object or specimen 514 through the immersion fluid 513 to Mangin mirror element 512, reflect from the second surface of 20 concave spherical reflector 511 onto the Mangin mirror element 512, and transmit through concave spherical reflector 511 to form an intermediate image 515 after concave spherical reflector 511. The field lens group 502 comprises a single field lens 510 in this aspect 25 of the design.

The focusing lens group 501 employs multiple lens elements, in this aspect the six lens elements 504, 505, 506, 507, 508, and 509, which may all be formed from a single type of material. The focusing lens 30 group 501 collects light from the field lens group

502, including the intermediate image 515. An aperture or mask can be placed at this aperture stop 516 to limit or modify the NA of the objective. The design presented in FIG. 5 generally offers the same
 5 advantages and flexibility described with respect to the design of FIG. 3. The lens prescription for this embodiment is shown in Table 3.

Table 3. Prescription for lenses for the design of FIG. 5

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.0
1	Infinity	14.0000		9.0
STO	Infinity	-14.0000		8.5
3	9.8113	2.5000	Fused silica	8.9
4	16.0993	0.5000		8.2
5	24.5090	1.2500	Fused silica	8.1
6	6.4363	3.5000		7.5
7	-4.6748	2.1162	Fused silica	7.6
8	-5.7355	0.5000		9.3
9	15.5382	2.5000	Fused silica	10.5
10	-48.2247	0.5000		10.4
11	9.5400	2.2500	Fused silica	9.9
12	39.5324	3.0432		9.3
13	Infinity	1.5000		7.2
14	-12.0978	3.3227	Fused silica	6.5
15	-10.1308	3.9848		5.9
16	4.1943	1.2500	Fused silica	2.6
17	-74.2314	2.5000		1.9
18	Infinity	0.0000		1.7
19	18.2106	4.0512	Fused silica	1.7
20	12.5801	6.7677		4.4
21	53.8539	4.7121	Fused silica	15.0
22	Infinity	-4.7121	MIRROR	17.8
23	53.8539	-6.7677		20.4
24	12.5801	-4.0512	Fused silica	21.7
25	18.2106	4.0512	MIRROR	27.7
26	12.5801	6.7677		19.4
27	53.8539	4.7121	Fused silica	8.1
28	Infinity	0.3000	Immersion fluid	0.6
IMA	Infinity		Immersion fluid	0.2

Another aspect of the design presents an immersion objective having ten elements. This aspect of the design is presented in FIG. 6. One difference between the design of FIG. 6 and that of FIG. 4 is the 5 addition of a small immersion lens in front of the catadioptric group. The immersion liquid 614 is located to the right of lens 613. The objective of the design of FIG. 6 is corrected over a bandwidth from between approximately 266 to 436 nm, and has a 10 field size of approximately 0.075 mm. The design of FIG. 6 again provides a relatively high approximately 1.2 numerical aperture assuming pure water is used as an immersion substance. Again, other immersion substances could be used with higher refractive 15 indices to further increase the NA. Worst case polychromatic wavefront error for the FIG. 6 design is approximately 0.045 waves.

From FIG. 6, the catadioptric group 603 includes an immersion lens 613, Mangin mirror element 612, 20 which is a reflectively coated lens element, and a concave spherical reflector 611, also a reflectively coated lens element. Both Mangin mirror element 612 and concave spherical reflector 611 have central optical apertures where reflective material is absent. 25 The absence of reflective material from the center of these components allows light to pass from the object and immersion liquid 614, through immersion lens 613, through Mangin mirror element 612, reflect from the second surface of concave spherical reflector 611 onto 30 the Mangin mirror element 612, and transmit through

concave spherical reflector 611 to form an intermediate image 615 after concave spherical reflector 611. Field lens group 602 comprises a single field lens 610 in this aspect of the design.

- 5 Note that borders for immersion liquid 614 are not specifically shown in this view; it is understood that immersion liquid 614 contacts immersion lens 613 and may be disposed adjacent to the surface of the specimen, not shown in this view.

- 10 The focusing lens group 601 employs multiple lens elements, in this aspect the six lens elements 604, 605, 606, 607, 608, and 609, which may all be formed from a single type of material. The focusing lens group 601 collects light from the field lens group 15 602, including the intermediate image 615. An aperture or mask can be placed at the aperture stop (not shown) to limit or modify the NA of the objective.

- 20 The lens prescription for this embodiment is shown in Table 4.

Table 4. Prescription for lenses for the design of FIG. 6

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.0
1	Infinity	21.0000		8.9
STO	Infinity	-21.0000		8.5
3	33.3993	2.0000	Fused silica	8.9
4	-15.0280	0.5000		8.8
5	14.6458	1.5000	Fused silica	8.0
6	5.6019	4.7962		7.0
7	-5.0202	2.4398	Fused silica	6.9

8	-9.5561	0.5000		8.4
9	31.6324	2.0000	Fused silica	9.0
10	-19.8335	0.5000		9.2
11	36.6869	2.0000	Fused silica	9.2
12	-312.7053	0.5000		9.0
13	5.5701	2.2500	Fused silica	8.6
14	13.6079	8.0205		8.0
15	1.3437	1.2495	Fused silica	1.7
16	2.2515	1.4000		0.7
17	Infinity	0.9995		2.0
18	20.3068	3.3979	Fused silica	30.0
19	16.7118	7.3529		26.0
20	-123.1263	4.1188	Fused silica	25.0
21	-84.9933	-4.1188	MIRROR	25.0
22	-123.1263	-7.3529		25.0
23	16.7118	-3.3979	Fused silica	26.0
24	20.3068	3.3979	MIRROR	30.0
25	16.7118	7.3529		26.0
26	-123.1263	4.1188	Fused silica	25.0
27	-84.9933	0.1000		25.0
28	1.7798	1.0000	Fused silica	2.0
IMA	Infinity		Immersion liquid	0.1

An alternate aspect of the present design presents an immersion objective with eleven separate elements. This aspect of the design is presented in FIG. 7. The difference between the design of FIG. 6 and that of FIG. 7 is the addition of a second field lens element, thus providing two field lens elements 710 and 711. The use of two field lens elements allows the immersion objective of the design of FIG. 7 to be corrected over a significantly wider bandwidth range, namely for bandwidths from approximately 266 to 800 nm. The objective of FIG. 7 provides a field size of approximately 0.100 mm and maintains the high approximately 1.1 numerical aperture assuming pure water is used as an immersion substance. Other immersion substances could be used with higher

refractive indices to further increase the NA. The worst case polychromatic wavefront error for the FIG. 7 design is approximately 0.06 waves.

From FIG. 7, the catadioptric group 703 includes
5 an immersion lens 714, Mangin mirror element 713,
which is a reflectively coated lens element, and a
concave spherical reflector 712, which is also a
reflectively coated lens element. Both Mangin mirror
element 713 and concave spherical reflector 712 have
10 central optical apertures where reflective material is
absent. The absence of reflective material, in the
center of the components shown, allows light to pass
from the specimen (not shown) through immersion liquid
715 and immersion lens 714, to Mangin mirror element
15 713, reflect from the second surface of concave
spherical reflector 712 onto the Mangin mirror element
713, and transmit through concave spherical reflector
712 to form an intermediate image 717 after passing
through concave spherical reflector 712 and field lens
20 711. Field lens group 702 comprises two field lenses
710 and 711 in this aspect of the design, and again,
borders for the immersion liquid or immersion
substance 715 are not illustrated in this view.

The focusing lens group 701 employs multiple lens
25 elements, in this aspect the six lens elements 704,
705, 706, 707, 708, and 709, which may all be formed
from a single type of material. The focusing lens
group 701 collects light from the field lens group
702, including the intermediate image 717. An
30 aperture or mask can be placed at the aperture stop

718 to limit or modify the NA of the objective. The design presented in FIG. 7 has the advantages and flexibility described with respect to the design of FIG. 3. The lens prescription for this embodiment is 5 shown in Table 5.

Table 5. Prescription for lenses for the design of FIG. 7

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.0
1	Infinity	23.8352		9.4
STO	Infinity	-23.8352		8.8
3	-37.3943	2.5000	Fused silica	9.4
4	-11.9960	0.2500		9.5
5	8.4950	1.6973	Fused silica	8.7
6	5.5741	4.0000		7.6
7	-5.5468	1.5000	Fused silica	7.5
8	-7.5748	0.5000		8.4
9	23.0221	2.5000	Fused silica	8.7
10	-59.7532	0.5000		8.7
11	6.2006	4.0067	Fused silica	8.5
12	5.9410	3.0486		6.5
13	Infinity	1.2510		5.9
14	21.1594	2.5000	Fused silica	5.5
15	-8.3289	1.4531		5.0
16	2.0000	2.2340	Fused silica	3.2
17	4.8552	0.7494		1.4
18	Infinity	0.6996		0.7
19	-5.0128	1.5000	Fused silica	1.8
20	-3.3963	0.2500		3.2
21	17.8880	2.9998	Fused silica	25.0
22	14.3688	5.7794		21.5
23	-169.9762	4.0812	Fused silica	21.0
24	-79.2615	-4.0812	MIRROR	21.0
25	-169.9762	-5.7794		21.0
26	14.3688	-2.9998	Fused silica	21.5
27	17.8880	2.9998	MIRROR	25.0
28	14.3688	5.7794		21.5
29	-169.9762	4.0812	Fused silica	21.0
30	-79.2615	0.1000		21.0
31	2.9243	1.5000	Fused silica	3.5
IMA	Infinity		Immersion liquid	0.1

Still another aspect of the present design presents an immersion objective with eight separate elements. This aspect of the design is presented in FIG. 8. The differences between the design of FIG. 8 and that of FIGs. 6 and 7 are a different catadioptric arrangement, fewer lens elements, and different correction wavelength, allowing the immersion objective to be corrected over a bandwidth from approximately 190 to 198 nm and simultaneously provide a field size of approximately 0.050 mm. The design of FIG. 8 maintains the high approximately 1.2 numerical aperture assuming pure water is used as an immersion substance, and other immersion substances could be used with higher refractive indices to further increase the NA. The worst case polychromatic wavefront error for the FIG. 8 design is approximately 0.05 waves.

From FIG. 8, the catadioptric group 803 includes an immersion lens element 811, a Mangin mirror element 810, which is a reflectively coated lens element, and a concave spherical reflector 809, which is also a reflectively coated lens element. Mangin mirror element 810 has a central optical aperture where reflective material is absent. Concave spherical reflector 809 has a physical hole in the center of the element. The absence of reflective material in element 810 and the central hole in 809 allows light to pass from the specimen or object (not shown, but again positioned on the right side of the objective in the view shown), through immersion liquid 812, and

immersion lens 811, through Mangin mirror element 810, reflect from the second surface of concave spherical reflector 809 onto the Mangin mirror element 810, and transmit through concave spherical reflector 809 to

5 form an intermediate image 814 in proximity to concave spherical reflector 809 and field lens 808. Field lens group 802 comprises one field lens 808 in this aspect of the design.

The focusing lens group 801 employs multiple lens elements, in this aspect the four lens elements 804, 10 805, 806, and 807, which may all be formed from a single type of material. The focusing lens group 801 collects light from the field lens group 802, including the intermediate image 814. An aperture or 15 mask can be placed at the aperture stop 815 to limit or modify the NA of the objective. The design presented in FIG. 8 has the advantages and flexibility described with respect to the design of FIG. 3. The lens prescription for this embodiment is shown in 20 Table 6.

Table 6. Prescription for lenses for the design of FIG. 8

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.0
1	Infinity	18.0000		7.3
2	Infinity	-18.0000		6.7
3	21.6009	2.2500	Fused silica	7.3
4	-21.6009	0.8283		7.1
5	5.0457	2.9908	Fused silica	6.1
6	3.0474	2.5000		4.0
7	-3.4102	2.4345	Fused silica	3.6
8	-5.2993	0.0000		4.1

STO	Infinity	0.0000		4.1
10	Infinity	0.5000		4.1
11	3.4327	4.1869	Fused silica	4.1
12	2.0000	5.1795		2.2
13	3.1184	1.5000	Fused silica	1.8
14	-17.0312	0.5000		1.4
15	15.8489	3.0000		0.0
16	10.9156	8.9489		0.0
17	5.5736	-8.9489	MIRROR	4.8
18	10.9156	-3.0000	Fused silica	20.2
19	15.8489	3.0000	MIRROR	26.2
20	10.9156	8.9489		20.2
21	5.5736	5.0086	Fused silica	10.8
22	7.6963	0.0500		7.5
23	7.1686	2.7256	Fused silica	7.0
24	Infinity	0.1000	Immersion liquid	7.0
IMA	Infinity		Immersion liquid	0.1

An alternate aspect of the present design employs a cover glass over the specimen and the associated objective corrects for the nominal thickness cover 5 glass. An objective used for imaging purposes may be altered or reoptimized when using a cover glass, or alternately when using a cover glass in combination with an immersion liquid. Use of a cover glass may be particularly beneficial during inspection of 10 biological materials. This aspect of the design is presented in FIG. 9. The objective illustrated is optimized for a nominal cover glass thickness of 0.17 mm and is corrected over a bandwidth from approximately 266 to 436 nm, with a field size of 15 approximately 0.150 mm. The design of FIG. 9 maintains the high approximately 0.9 numerical aperture. Worst case polychromatic wavefront error for the FIG. 9 design is approximately 0.04 waves.

From FIG. 9, the catadioptric group 903 includes a Mangin mirror element 912, a reflectively coated lens element, and concave spherical reflector 911, also a reflectively coated lens element. Mangin
5 mirror elements 911 and 912 have central optical apertures free of reflective material. The absence of reflective material from elements 911 and 912 allows light to pass from the object or specimen 914, borders not shown, through cover glass 913, through Mangin
10 mirror element 912, reflect from the second surface of concave spherical reflector 911 onto the Mangin mirror element 912, and transmit through concave spherical reflector 911 to form an intermediate image 915 in proximity to concave spherical reflector 911 and field
15 lens group 902. Field lens group 902 comprises one field lens 910 in this aspect of the design.

The focusing lens group 901 employs multiple lens elements, in this aspect the six lens elements 904, 905, 906, 907, 908, and 909, which may all be formed
20 from a single type of material. The focusing lens group 901 collects light from the field lens group 902, including the intermediate image 915. An aperture or mask can be placed at the aperture stop (not shown) to limit or modify the NA of the
25 objective. The design presented in FIG. 9 again has the advantages and flexibility described with respect to the design of FIG. 3. The lens prescription for this embodiment is shown in Table 7.

Table 7. Prescription for lenses for the design of
FIG. 9

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.00
1	Infinity	17.4042		9.05
STO	Infinity	-17.4042		8.50
3	21.8272	2.0000	Fused silica	9.03
4	-30.1966	0.5000		8.85
5	21.2221	1.2500	Fused silica	8.38
6	7.4018	5.4944		7.65
7	-6.3015	2.3948	Fused silica	7.58
8	-14.2766	0.5000		8.88
9	49.7005	2.0000	Fused silica	9.37
10	-21.4447	0.5000		9.58
11	19.2912	2.0000	Fused silica	9.64
12	-132.2143	0.5000		9.46
13	6.6946	2.2500	Fused silica	8.91
14	17.2123	7.9753		8.20
15	Infinity	0.0000		2.84
16	1.9458	1.2495	Fused silica	2.52
17	6.2708	0.6796		1.68
18	Infinity	0.0000		0.79
19	Infinity	0.9995		0.79
20	18.0063	3.0198	Fused silica	26.00
21	13.5996	6.2718		21.00
22	Infinity	4.9453	Fused silica	21.00
23	-78.6167	-4.9453	MIRROR	21.00
24	Infinity	-6.2718		21.00
25	13.5996	-3.0198	Fused silica	21.00
26	18.0063	3.0198	MIRROR	26.00
27	13.5996	6.2718		21.00
28	Infinity	4.9453	Fused silica	21.00
29	-78.6167	0.3006		21.00
30	Infinity	0.0000		0.41
31	Infinity	0.1700	Fused silica (Cover glass)	0.41
IMA	Infinity		Fused silica	40.00

The actual thickness of cover glass may vary from
5 the nominal value of 0.17 mm. Effective imaging
suggests that the cover glass thickness may vary over
a range of ± 0.020 mm from the nominal and still employ
an objective similar to that shown. The system may

compensate for changes in the thickness of the cover glass by adjusting the spacing between the focusing lens group 901, the field lens group 902, and the catadioptric group 903. Table 8 summarizes the
 5 compensation.

Table 8. Compensation for variations in the cover glass thickness of the design in FIG 9.

Cover glass thickness (mm)	Object focus shift (mm)	Focusing lens group to Field lens group separation change (mm)	Field lens group to Catadioptric group separation change (mm)	Resulting polychromatic Strehl
0.150	- 0.0086	0.0505	0.0233	0.86
0.160	- 0.0043	0.0252	0.0116	0.92
0.170	0.0	0.0	0.0	0.93
0.180	0.0042	-0.0251	-0.0115	0.90
0.190	0.0085	-0.0502	-0.0229	0.84

10

As can be seen from the table, decreasing the cover glass thickness can be corrected by increasing the distances between the focusing lens group, field lens group, and catadioptric group. Using this approach,
 15 element shifts may be performed by fixing the field lens group in a rotating ring and attaching the ring

by threads or other rotary attachment device to the catadioptric group and focusing lens group. With threads of the proper pitch and direction on either side of the rotating ring, proper compensation can be
5 achieved using one mechanical rotation motion. In operation, an operator or device may cause the ring to be rotated, thereby changing the distance between the field lens group and the focusing lens group, and simultaneously between the field lens group and the
10 catadioptric group.

In addition, the change in distance separation between the focusing lens group and the field lens group can be made twice the change of the separation between the field lens group and catadioptric group
15 with only a small performance penalty.

This technique of adjusting the air gaps between the focusing lens group, field lens group, and catadioptric group can also compensate for variations in the refractive index of the immersion fluid used in
20 the designs of FIGs 3-8.

An alternate aspect of the present design presents a self corrected varifocal imaging optics system having five elements and being corrected over a wavelength range from 266-800 nm using two glass
25 materials, fused silica and calcium fluoride. One aspect of such an objective design is shown in FIG. 10. This optical system can produce variable focal lengths from 200 mm to as large as desired. The only limitation is the total length of the system.

From FIG. 10, the varifocal optics include a fixed focusing group 1001 and a moving imaging group 1002. The fixed focusing group 1001 is located a desired distance from the objective exit pupil 1003.

- 5 In this aspect of the invention, this separation distance is set to 100 mm. A 100 mm separation distance allows for insertion of beam splitters, phase plates, or filters between the objective and varifocal optics. The fixed focusing group 1001 includes two
 10 lenses 1004 and 1005 in this aspect of the invention. The moving imaging group 1002 includes three lens elements 1006, 1007, and 1008.

The lens prescription for the aspect of the invention illustrated in FIG. 10 is presented in Table
 15 9.

Table 9. Prescription for lenses for the design of FIG. 10

Surf	Radius	Thickness	Glass	Diameter
OBJ	Infinity	Infinity		0.00
STO	Infinity	100.0000		8.10
2	51.6824	4.5000	Calcium fluoride	11.00
3	-22.5040	0.1000		10.84
4	-22.7121	3.0000	Fused silica	10.81
5	Infinity	102.1114		10.67
6	25.2044	3.0000	Fused silica	5.09
7	28.1765	2.0000		4.79
8	-31.3982	3.0000	Calcium fluoride	4.66
9	8.2051	1.5000		4.65
10	9.2578	3.0000	Fused silica	5.07
11	37.0927	25.0000		5.05
12	Infinity	1.0000	Fused silica	6.41
13	Infinity	1.0000		6.45
IMA	Infinity			6.51

Total focal length of the system may be altered by changing the focal length of either the focusing group 1001 or the imaging group 1002. Increasing the focal length of the focusing group 1001 will increase 5 the thickness of Surface 11 at the smallest desired focal length. Increasing the focal length of the focusing group 1001 will concurrently increase the thickness of Surface 11 at the largest desired focal length. Modification of the distance between the 10 imaging group 1002 and the fixed focusing group 1001 changes the focal length of the varifocal optics. When the distance between focusing group 1001 and imaging group 1002 changes, the distance between the imaging group 1002 and the detector 1010 must also 15 change to bring the image into focus. Window 1009 is typically fixed to the front of the detector to protect the detector and limit photocontamination. The focal length of the varifocal optics and the distances change according to Table 10.

20 **Table 10. Lens group position and focal length changes for the design of FIG. 10**

EFFL (Focal Length, mm)	Magnification using 4.5mm focal length objective	Thickness of Surface 5 (mm)	Thickness of Surface 11 (mm)
225	50X	102.11	25.00
450	100X	89.27	100
900	200X	82.89	250

1800	400X	79.69	555
3600	800X	78.01	1250

The distance between the focusing group 1002 and the detector 1010 may be achieved by using movable mirrors or by moving the detector 1010. Moving the detector
5 1010 may be easiest when small focal lengths are desired. However, with large focal lengths, the necessary distance can increase rapidly. In the presence of a rapidly increasing distance, use of moving mirrors reduces the space required for
10 refocusing.

"Figure four" or "trombone mirror" geometries can assist in space reduction and providing effective inspection using the objectives presented. One possible "figure four" geometry is shown in FIG. 11.
15 Light first enters fixed focusing group 1101, comprising lenses 1101a and 1101b, and is focused to imaging group 1102, comprising lenses 1102a, 1102b, and 1102c. Light then reflects off reflective surfaces or mirrors 1103 and 1104 before reaching
20 detector 1105. The positions of mirrors 1103 and 1104 can be changed to increase or decrease the distance from imaging lens group 1102 to fixed detector 1105. This effectively brings the image into focus.

A "trombone geometry" may also be employed, and
25 one possible design is shown in FIG. 12. Light enters fixed focusing group 1201, including lenses 1201a and

1201b, and is focused to imaging group 1202, comprising lenses 1202a, 1202b, and 1202c . Light then reflects from mirrors 1203, 1204, and 1205 before reaching detector 1206. The position of mirror group 5 1207, which in this embodiment is composed of mirrors 1204 and 1205, can be changed to increase or decrease the distance from imaging lens group 1202 to fixed detector 1206. The effect of this aspect of the design is to more adequately bring the image into 10 focus.

The varifocal optics described in this embodiment can be of the same design as presented in Table 9. The moving mirrors only serve to adjust the air space between lens group 1202 and the detector. In the case 15 where the varifocal optics are of the design presented in Table 9, the air space between the lens group 1202 and the detector can be adjusted according to the values in Table 10.

20 The present system design may be employed in various environments, including but not limited to lithography, microscopy, biological inspection, medical research, and the like.

25 The design presented herein and the specific aspects illustrated are meant not to be limiting, but may include alternate components while still incorporating the teachings and benefits of the invention, namely the small design using immersion liquid or liquids having a high NA, up to a range of 1.2, able to be employed in various wavelengths using

different illumination modes. While the invention has thus been described in connection with specific embodiments thereof, it will be understood that the invention is capable of further modifications. This 5 application is intended to cover any variations, uses or adaptations of the invention following, in general, the principles of the invention, and including such departures from the present disclosure as come within known and customary practice within the art to which 10 the invention pertains.

The design presented herein and the specific aspects illustrated are meant not to be limiting, but may include alternate components while still incorporating the teachings and benefits of the 15 invention, namely the small design having a high NA able to be employed in various wavelengths using different illumination modes. While the invention has thus been described in connection with specific embodiments thereof, it will be understood that the 20 invention is capable of further modifications. This application is intended to cover any variations, uses or adaptations of the invention following, in general, the principles of the invention, and including such departures from the present disclosure as come within 25 known and customary practice within the art to which the invention pertains.